

# Surface Acoustic Solitary Waves

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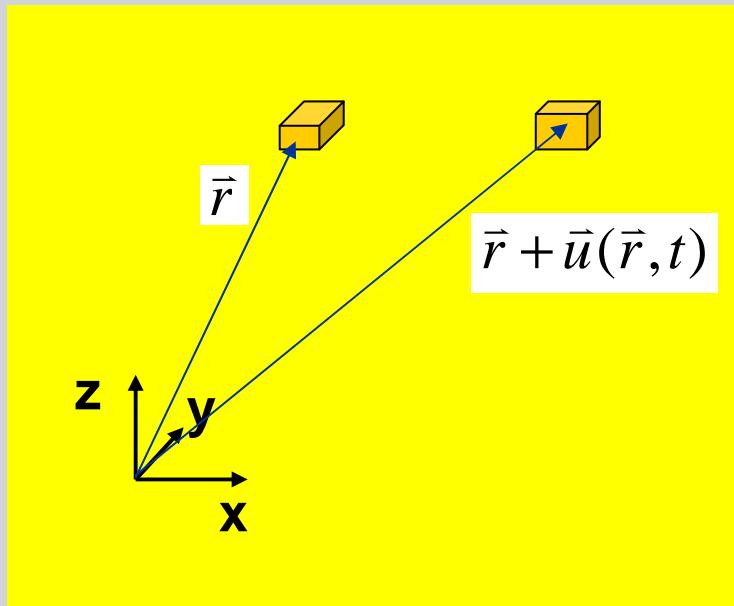


# Outline

- Linear surface acoustic waves (SAWs)
- Pulse evolution on homogeneous elastic media
- Solitary wave pulses on coated substrates
- Edge acoustic waves

# Elasticity Theory

Displacement field:  $\vec{u}(\vec{r}, t)$



$\vec{r}$  : Position of mass element in undeformed medium

$\vec{r} + \vec{u}(\vec{r}, t)$  :

Position of same mass element in deformed medium

# Elasticity Theory

Displacement field:

$$\vec{u}(x, z, t)$$

Displacement gradients:

$$u_{\alpha,\beta} = \frac{\partial u_\alpha}{\partial x_\beta}$$

Piola-Kirchhoff stress tensor:

$$T_{\alpha\beta} = C_{\alpha\beta\gamma\delta} u_{\gamma,\delta} + \frac{1}{2} S_{\alpha\beta\gamma\delta\epsilon\zeta} u_{\gamma,\delta} u_{\epsilon,\zeta} + O(u^3)$$

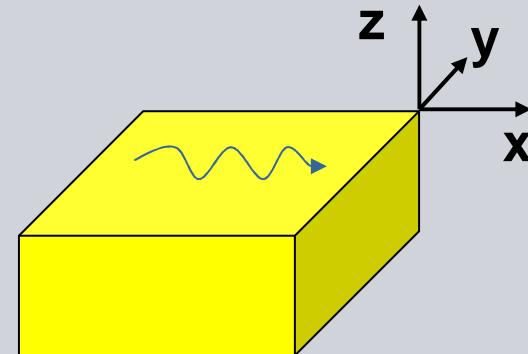
Equation of motion:

$$\rho \ddot{u}_\alpha = T_{\alpha\beta,\beta}$$

Boundary conditions:

$$T_{\alpha 3} \Big|_{z=0} = 0$$

$$u \xrightarrow[z \rightarrow \infty]{} 0$$

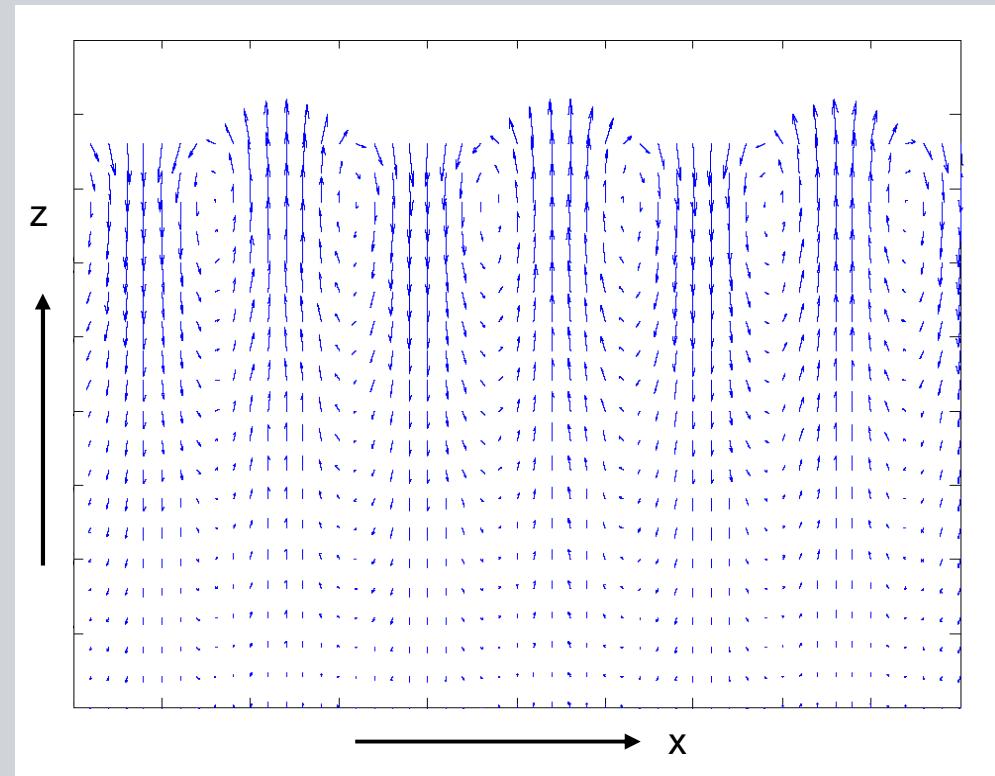


$$\begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

# Linear SAW

Displacement field:

$$u_\alpha(x, z, t) = \exp[iq(x - v_R t)] w_\alpha(z | q) + c.c.$$



depth profile

$$u_1(x, z, t) = \cos[q(x - v_R t)] W_1(z | q)$$
$$u_3(x, z, t) = \sin[q(x - v_R t)] W_3(z | q)$$

# Applications

## Wavelength

km

Geophysics (seismics, earthquakes)

$\mu\text{m}$

Non-destructive testing

Sensors

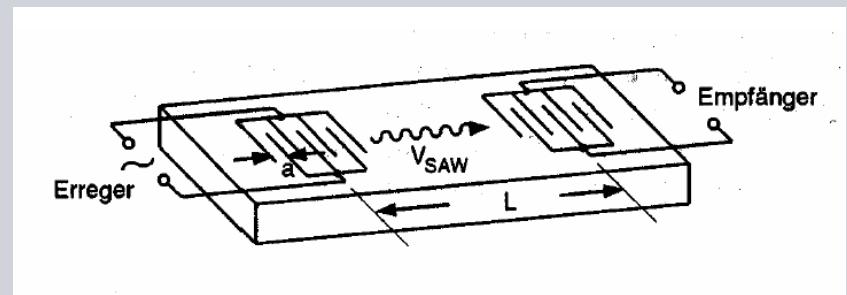
**Electronic devices**

**(frequency filters, delay lines,...)**

Source: IMTEK, Uni Freiburg

nm

Surface physics



# Nonlinearity / Dispersion

## Nonlinearity

Piola-Kirchhoff stress tensor:  $(T_{\alpha\beta})$

$$T_{11} = C_{1111}u_{1,1} + \dots + \frac{1}{2}S_{111111}u_{1,1}u_{1,1} + \dots + O(u^3)$$

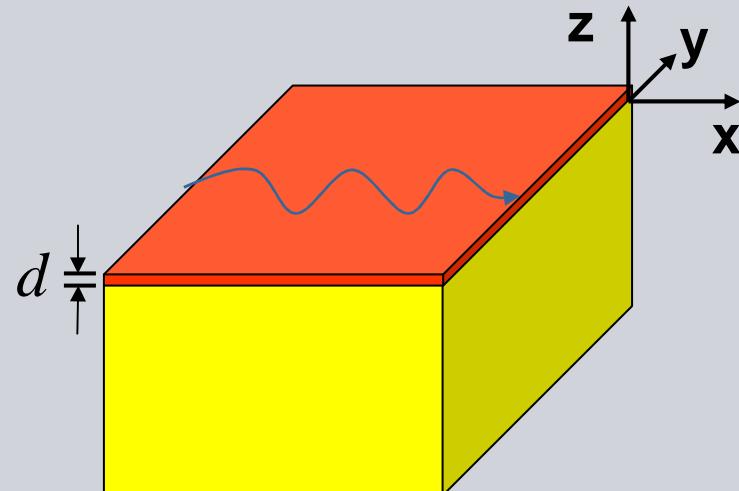
$$u_{\alpha,\beta} = \frac{\partial u_\alpha}{\partial x_\beta}$$
 displacement gradients

## Dispersion

due to coating of substrate (**S**)  
by film (**F**) of different material



Phase velocity depends on wavelength



$$\text{SAW frequency: } \omega(q) = v_R q + \Delta_0 q^2 + \Delta_1 q^3 + O(q^4)$$

# Nonlinear Pulse Evolution

Nonlinearity is small:  $|u_{\alpha,\beta}| < 0.01$



Asymptotic expansion for displacement gradient:  $u_{\alpha,1} = \varepsilon u_{\alpha,1}^{(1)} + \varepsilon^2 u_{\alpha,1}^{(2)} + O(\varepsilon^3)$   
with “stretched” time coordinate:  $\tau$

Fourier transform of displacement gradients at the surface:

$$u_{\alpha,1}^{(1)}(x,0,t) = \int_0^\infty \exp[iq(x - v_R t)] B(q; \tau) \frac{dq}{2\pi} + c.c.$$

strain amplitude



**Evolution equation**  
for strain amplitudes

(Reutov, Kalyanasundaram, Lardner, Parker)

# Evolution Equation

for homogeneous medium (no dispersion):

$$i \frac{\partial}{\partial \tau} B(q) = q v_R \left[ \int_0^q F\left(\frac{k}{q}\right) B(k) B(q-k) dk + 2 \int_q^\infty \left(\frac{q}{k}\right) F\left(\frac{q}{k}\right)^* B(k) B(k-q)^* dk \right]$$

Depends on ratios of 2<sup>nd</sup>-order and  
3<sup>rd</sup>-order elastic moduli:

**Influence of anisotropy !**

**Non-local nonlinearity !**

# Evolution Equation

Evolution equation for **weakly dispersive SAW**:

$$i \frac{\partial}{\partial \tau} B(q) = q^2 \Delta_R(q) B(q)$$
$$+ q v_R \left[ \int_0^q F\left(\frac{k}{q}\right) B(k) B(q-k) dk + 2 \int_q^\infty \left( \frac{q}{k} \right) F\left(\frac{q}{k}\right)^* B(k) B(k-q)^* dk \right]$$

Evolution equation for **weakly dispersive BAW: KdV equation**

$$i \frac{\partial}{\partial \tau} B(q) = q^3 \Delta_B B(q) + q v_B \left[ \int_0^q B(k) B(q-k) dk + 2 \int_q^\infty B(k) B(k-q)^* dk \right]$$

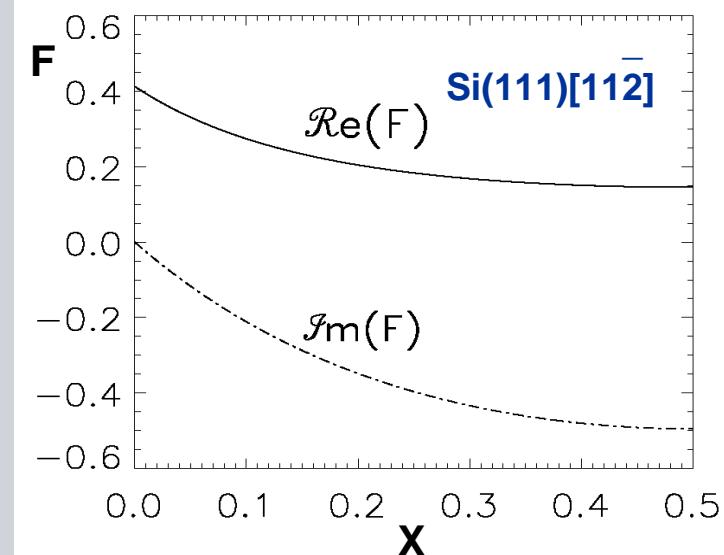
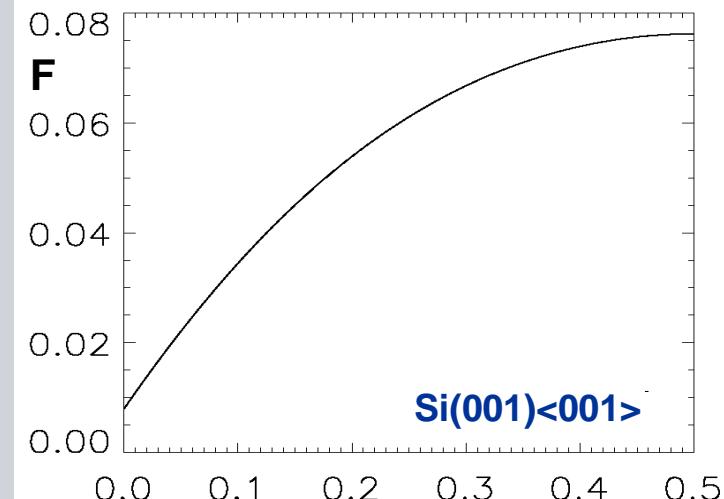
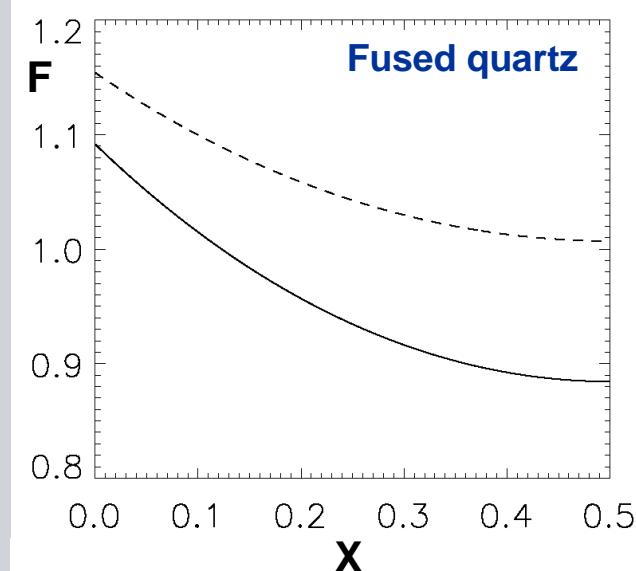


$$\frac{\partial}{\partial \tau} V - \Delta_B \frac{\partial^3}{\partial \xi^3} V + 2 v_B V \frac{\partial}{\partial \xi} V = 0$$

# Evolution Equation

Function  $F$  in evolution equation  
for  $u_{1,1}$ :

$$F(X) = F(1-X)$$



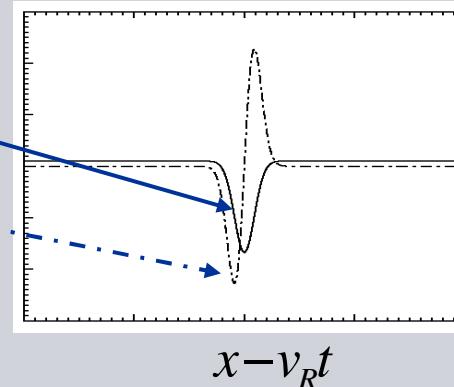
# Pulse Evolution without Dispersion

Initial surface elevation profile

surface slope

$$u_3(x,0)$$

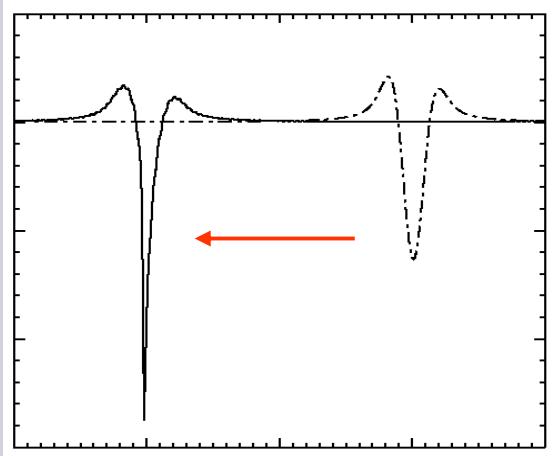
$$u_{3,1}(x,0)$$



$$x - v_R t$$

**Si(111)[112]**

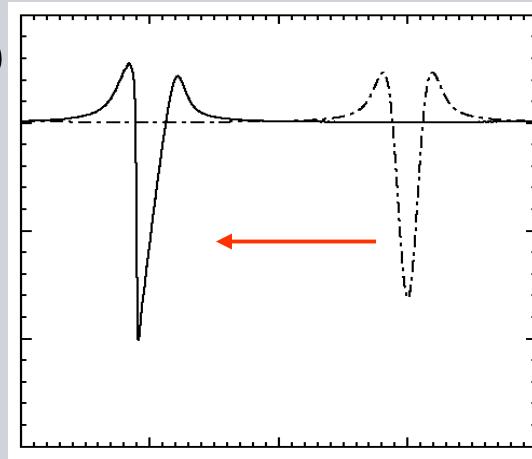
$$u_{1,1}(x,0)$$



$$x - v_R t$$

**Si(001)[100]**

$$u_{1,1}(x,0)$$

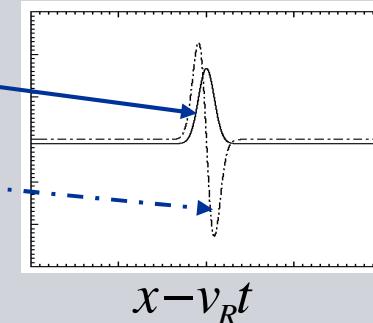


$$x - v_R t$$

# Pulse Evolution without Dispersion

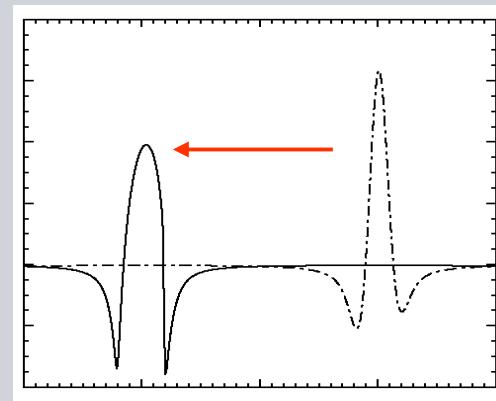
Initial surface elevation profile  $u_3(x,0)$

surface slope  $u_{3,1}(x,0)$



**Si(111)[112]**

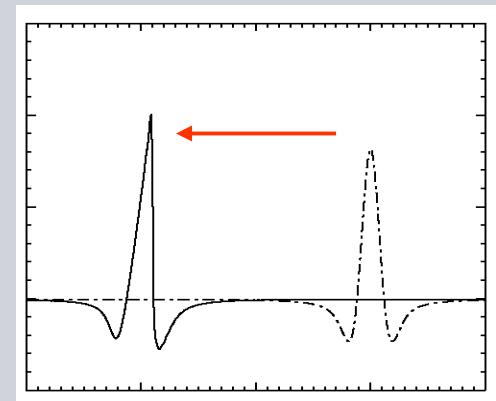
$u_{1,1}(x,0)$



$x - v_R t$

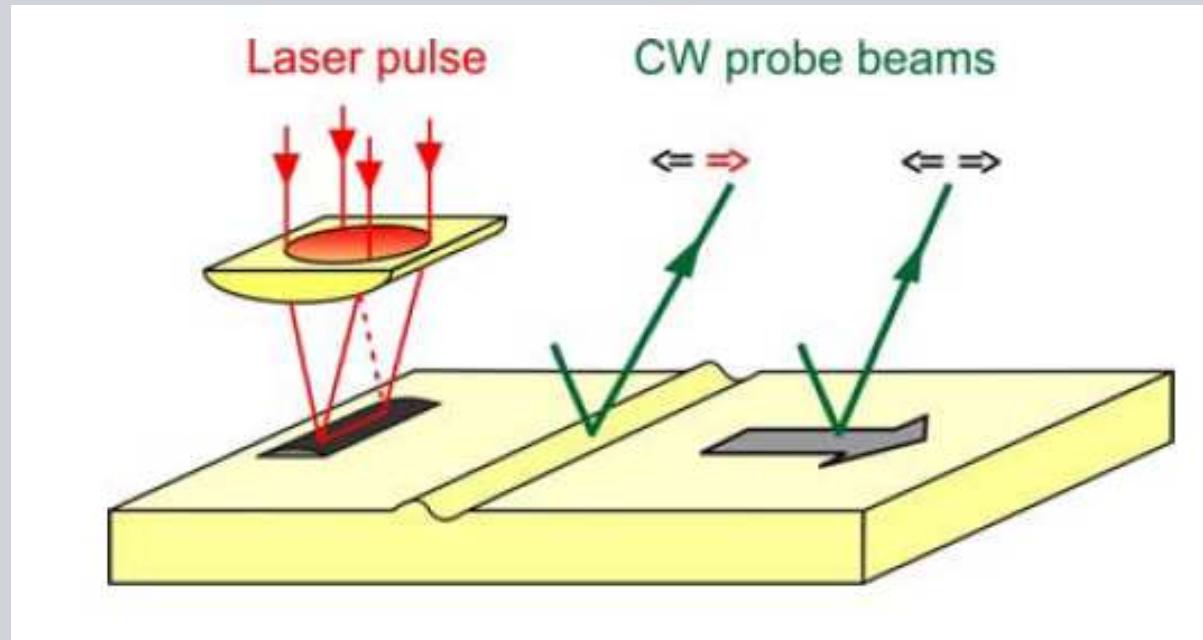
**Si(001)[100]**

$u_{1,1}(x,0)$



$x - v_R t$

# Laser Excitation

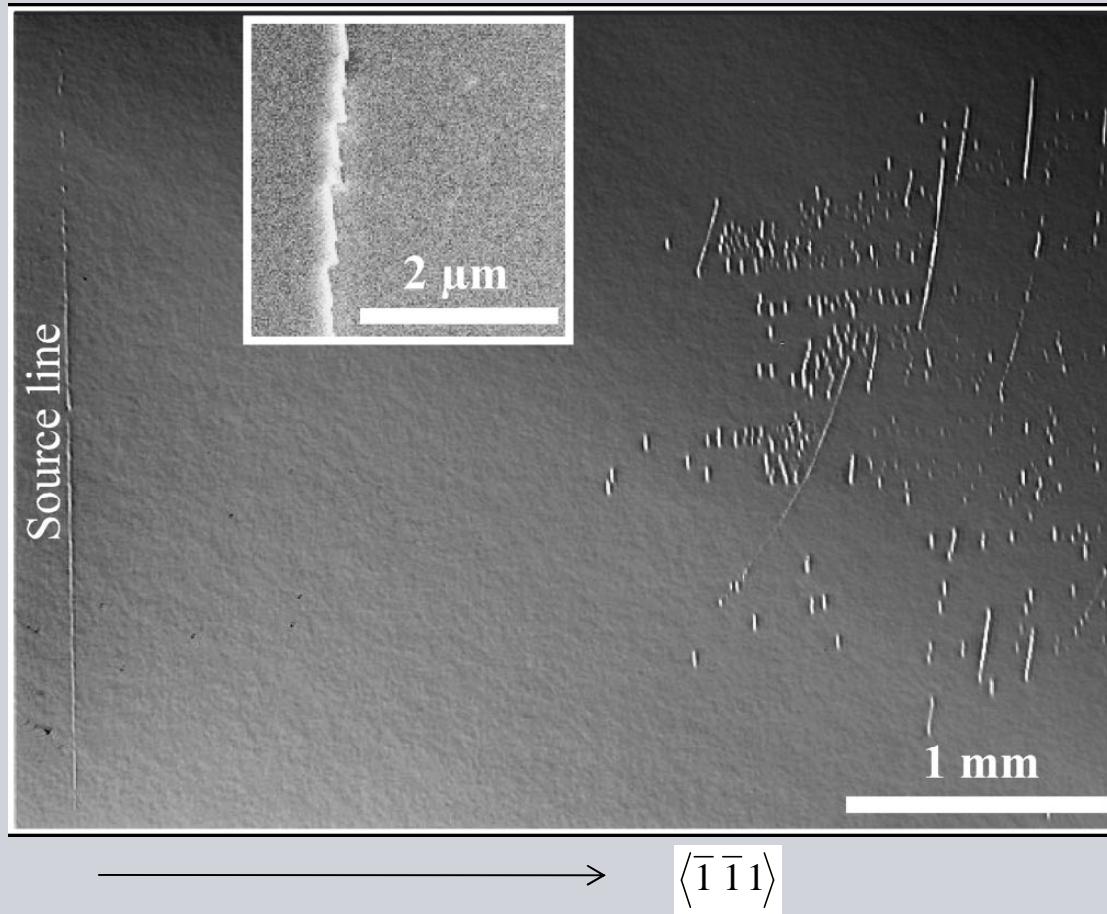


Experimental setup

A.M. Lomonosov, V.V. Kozhushko and P. Hess

# Crack formation

Optical microscope image of Si(112) surface after propagation of a nonlinear SAW pulse in the  $\langle -1 -1 1 \rangle$  direction

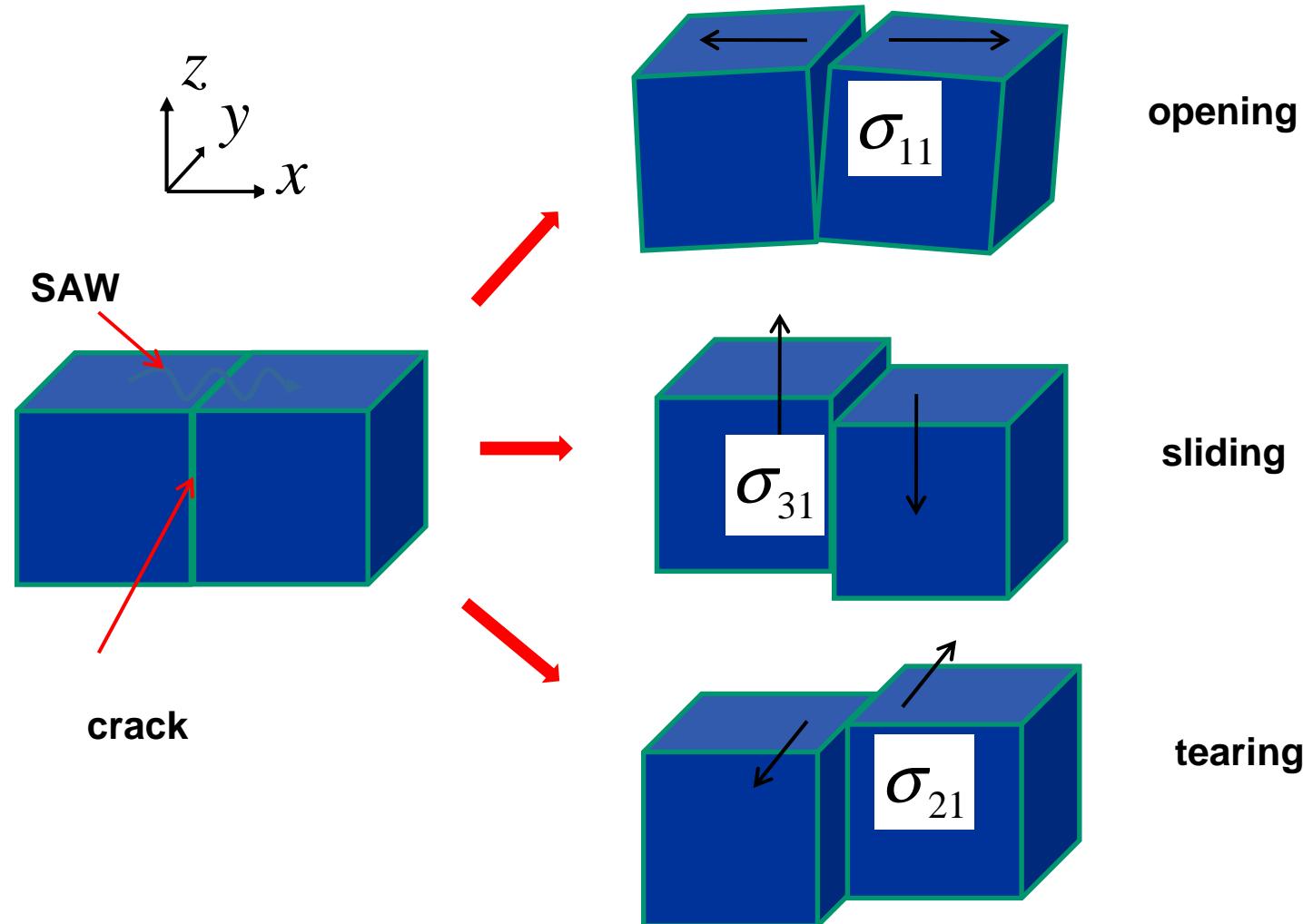


**V.V. Kozhushko,  
A.M. Lomonosov,  
and P. Hess**

PRL 98, 195505 (2007)

# Crack formation

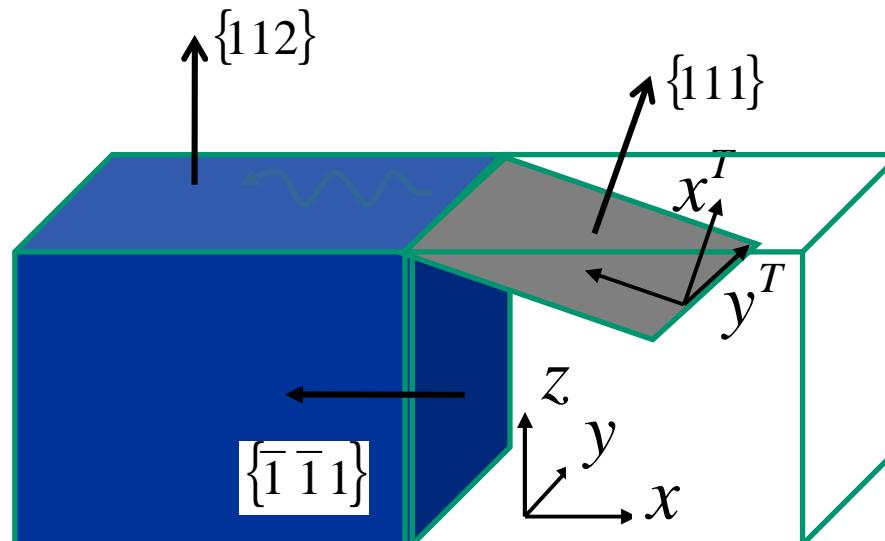
## Fracture modes of Si {111} surfaces



# Crack formation

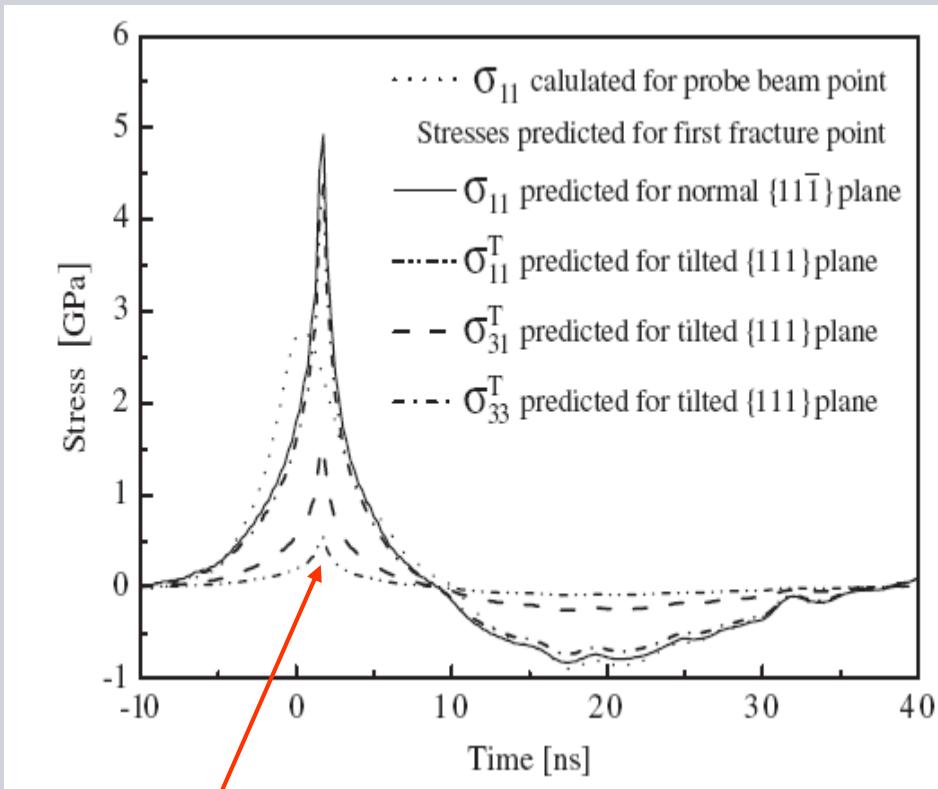
**Critical planes:**     $\{111\}$      $\{\bar{1}\bar{1}1\}$      $\{1\bar{1}\bar{1}\}$      $\{\bar{1}1\bar{1}\}$

**Example:** Si(112) surface



# Crack formation

Calculated stress at the Si(112) surface:



Pulse shape depends on excitation mechanism and elastic nonlinearity

V.V. Kozhushko,  
A.M. Lomonosov,  
and P. Hess

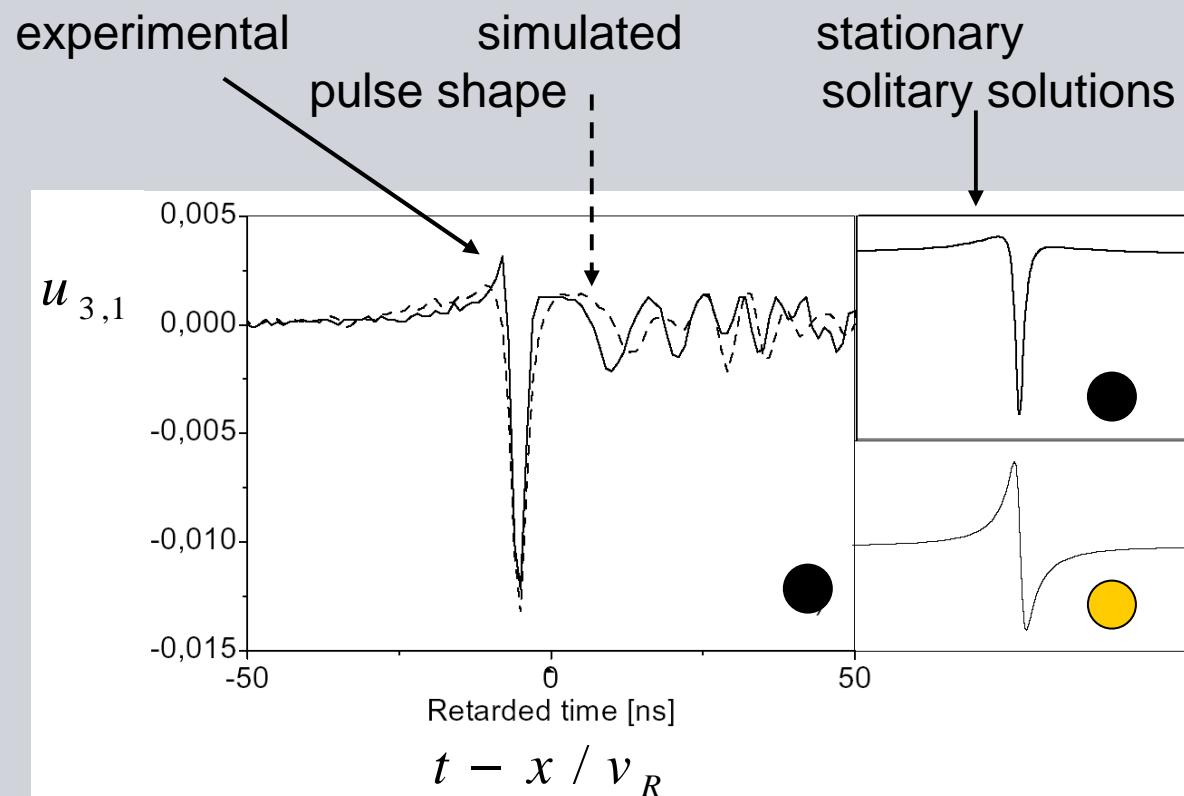
PRL 98, 195505 (2007)

Critical strength  
(Ab-initio calculations): **22 GPa**

Experimental  
strength: **5-7 GPa**

# Solitary Pulses

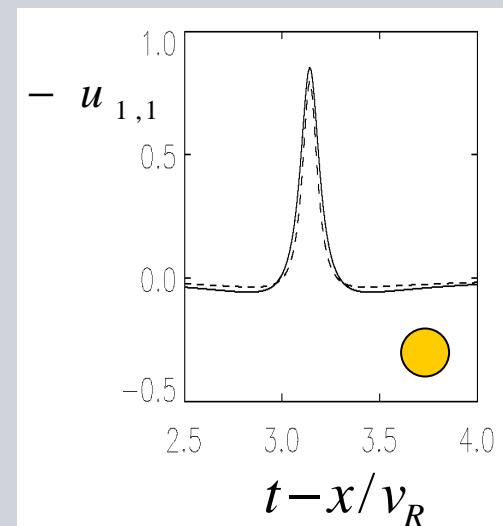
Pulse evolution after laser excitation  
**(Lomonosov & Hess)**



Stationary pulse shape  
calculated with

full  $F(X)$  —

$F(X)$  replaced by  $F(1/2)$  ---



● **Si(111)[ $\bar{1}\bar{1}2$ ]**

● **Si(001)[ $\bar{1}00$ ]**

# Solitary Pulses

2-parameter family:

$$u_{\alpha,1}^{(1)}(x,0,t) = K S_\alpha \left( K (x - v_R t \pm K v_R \tau - x_0) \right)$$

for linear dispersion law  $\omega(q) - v_R q = \Delta_0 q^2$

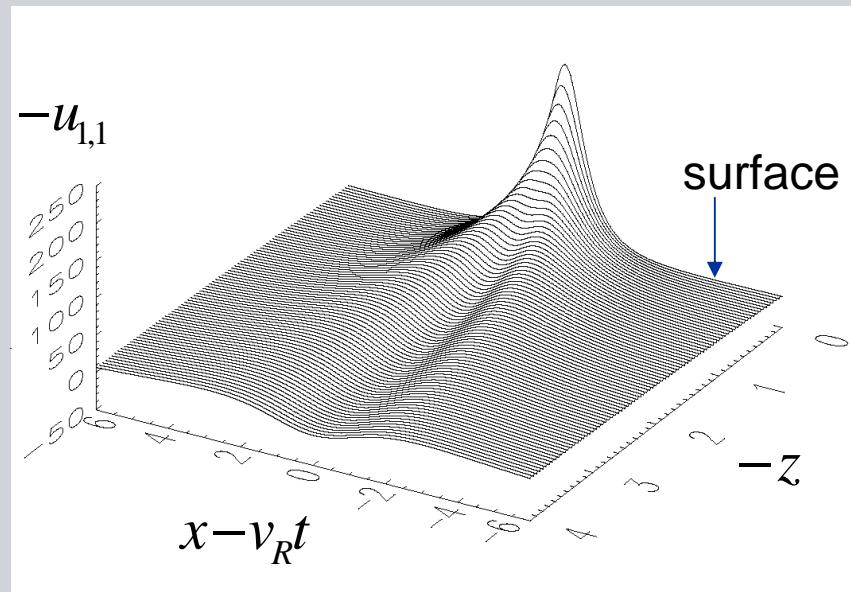
$$u_{\alpha,1}^{(1)}(x,0,t) = K S_\alpha \left( \sqrt{K} (x - v_R t \pm K v_R \tau - x_0) \right)$$

for linear dispersion law  $\omega(q) - v_R q = \Delta_1 q^3$

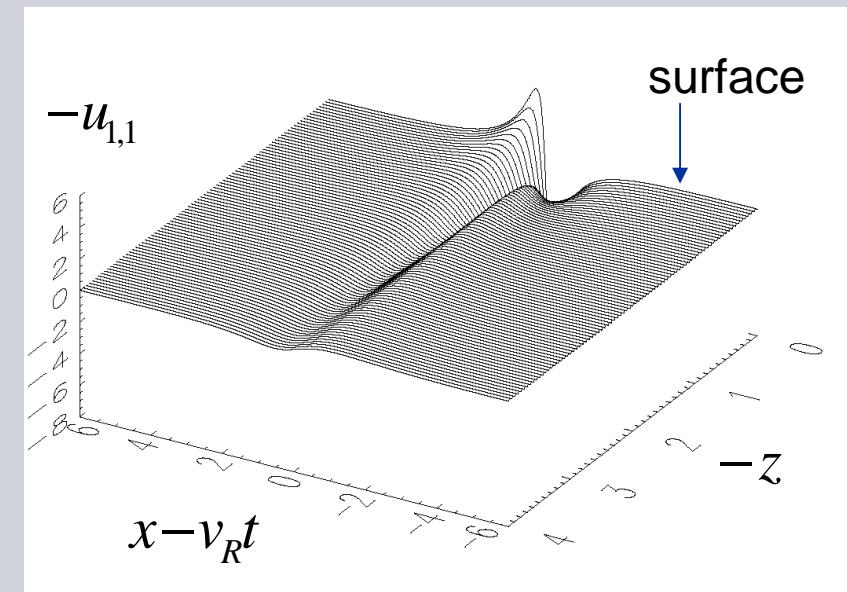
Can be computed as limiting cases  
of periodic pulse-train solutions.

# Depth Profile

## Strain / Particle Velocity



Fused silica

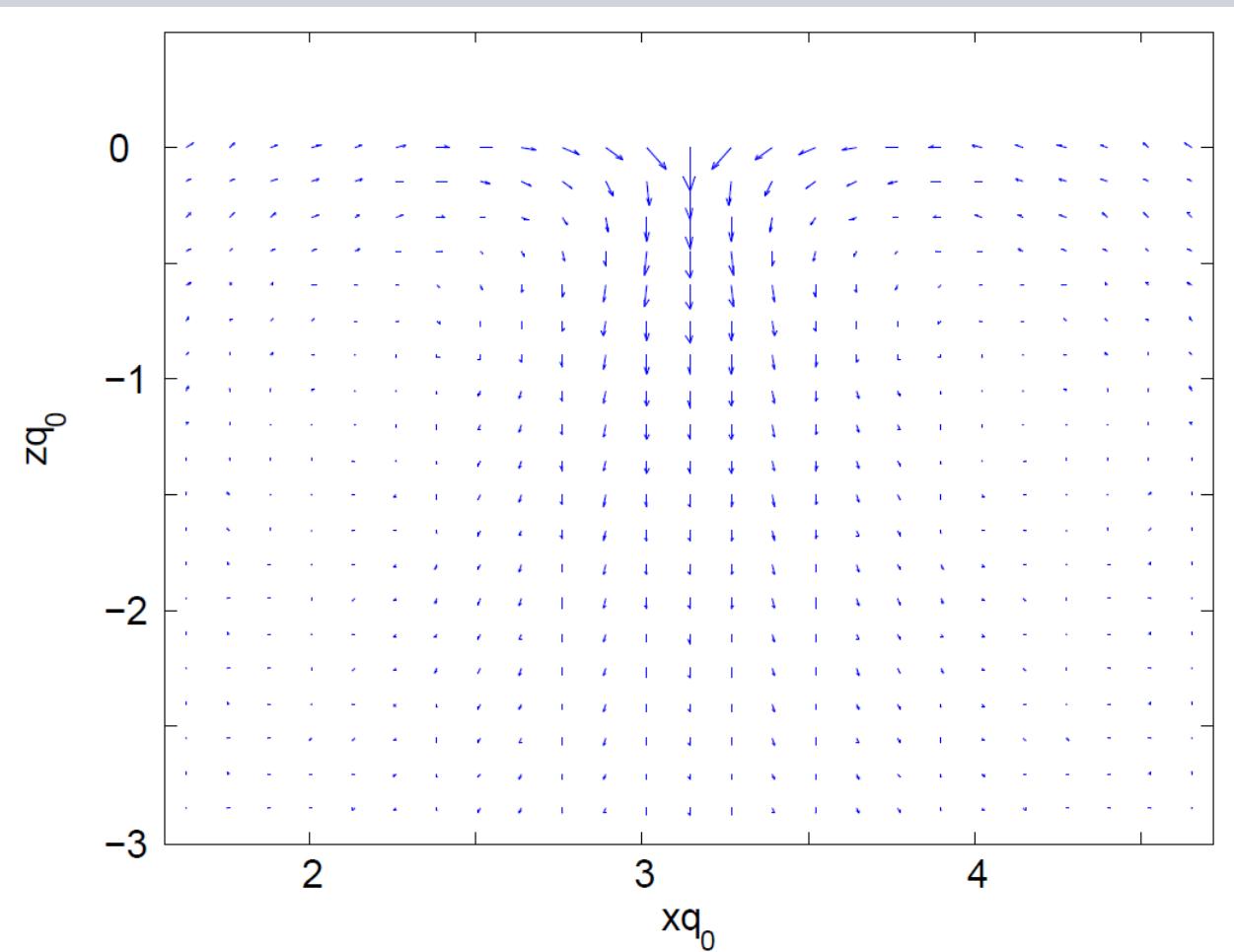


Si(111)[ $\bar{1}\bar{1}2$ ]

# Depth Profile

## Displacement Pattern

Fused silica



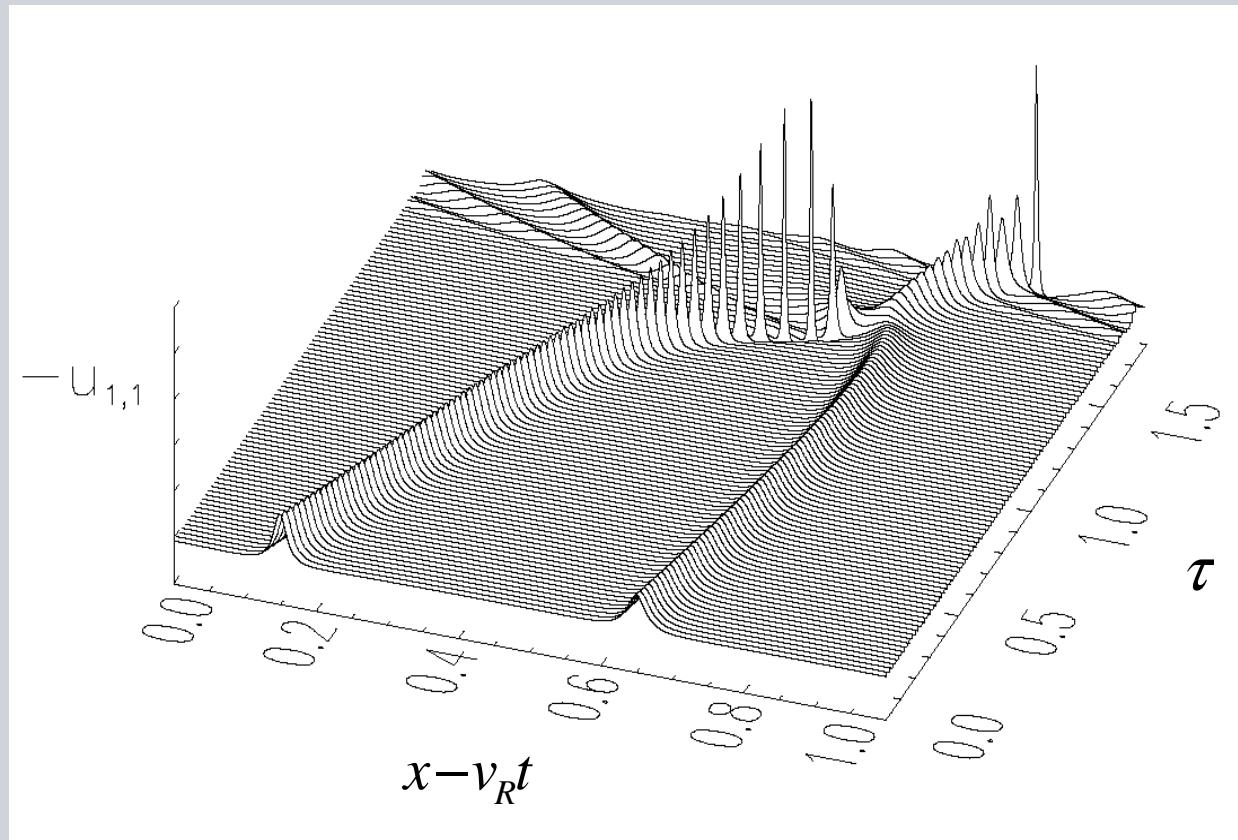
# Solitary Pulses

## Definitions:

**Solitary pulses** propagate without change of their shape.

**Solitons** are solitary pulses which survive collisions with each other as intact pulses.

# Pulse Collisions



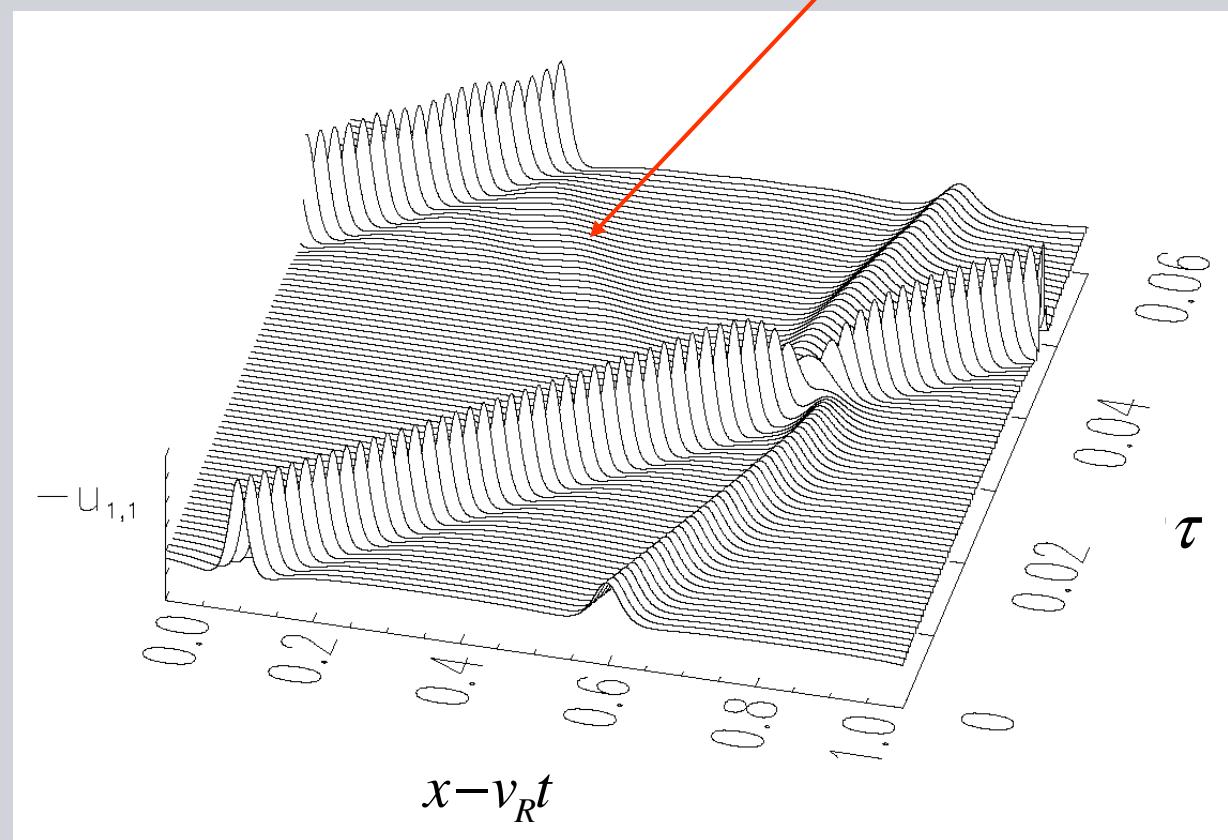
**Nonlinearity:**

$F = \text{const.}$

**Dispersion:**

$$\omega(q) - v_R q = \Delta_0 q^2$$

# Pulse Collisions



**Nonlinearity:**

$F = \text{const.}$

**Dispersion:**

$$\omega(q) - v_R q = \Delta_1 q^3$$

**Family of evolution equations:**

$$\frac{\partial}{\partial \tau} U = \frac{1}{4} (5\lambda - 1) \frac{\partial^3}{\partial \xi^3} U + (\lambda - 1) \hat{H} \left[ \frac{\partial}{\partial \xi} U \right] \frac{\partial}{\partial \xi} U + \frac{\partial}{\partial \xi} \left\{ \hat{H} \left[ U \frac{\partial}{\partial \xi} U \right] + (2\lambda - 1) U \hat{H} \left[ \frac{\partial}{\partial \xi} U \right] - \frac{4}{9} \lambda U^3 \right\}$$

has solitary wave solution **independent of parameter  $\lambda$  !**

$$U(\xi, \tau) = \frac{-3\sqrt{12\kappa}}{4\kappa(\xi - \kappa\tau - \xi_0)^2 + 3}$$

$\hat{H}$  : Hilbert transform w.r.t.  $\xi$

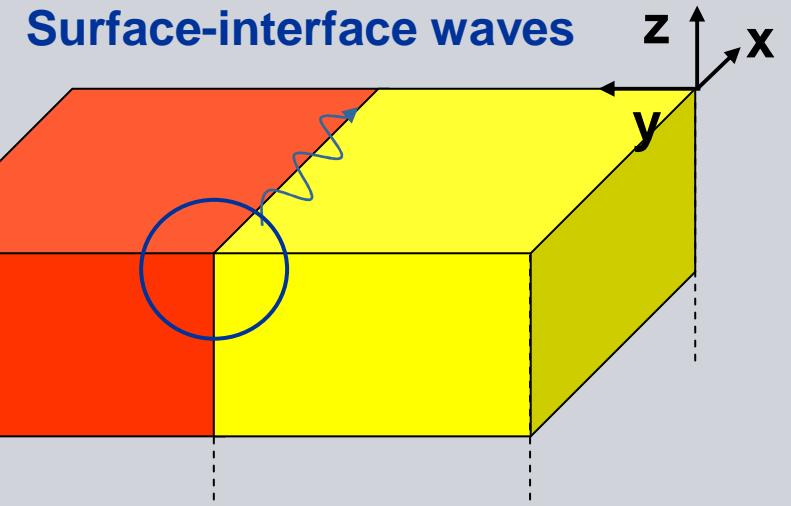
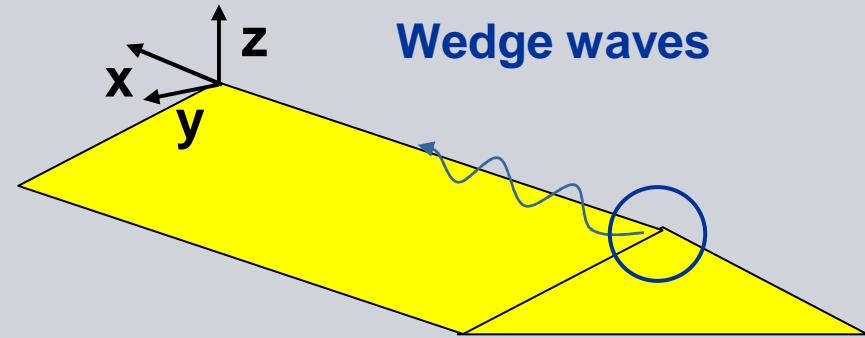
$\lambda=0$ : **Evolution equation for nonlinear dispersive SAW**  
 $U \propto u_3$ , approximation:  $F=\text{const.}$

$\lambda=1$ : **BO<sub>3</sub>-equation**  
has multi-soliton solutions.

# 1D Non-Dispersive Acoustic Waveguides

Displacement gradient associated with linear guided waves:

$$u_{\alpha,1}(x, y, z, t) = \exp[iq(x - vt)] w_{\alpha}(y, z | q) B(q) + c.c.$$

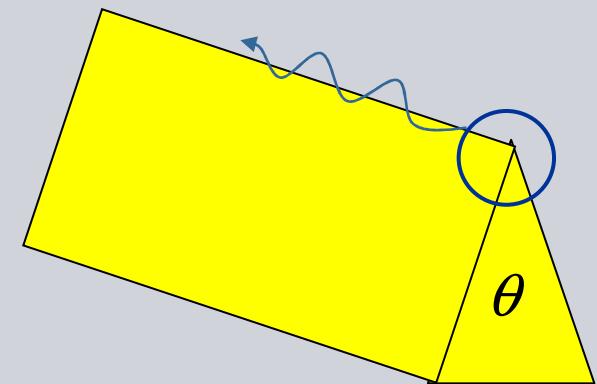


# Wedge Acoustic Waves

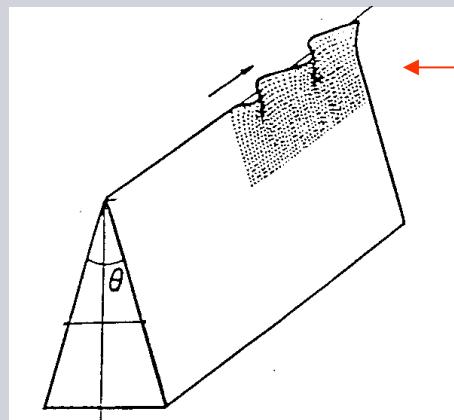
Predicted 1972 by

Lagasse  
(FEM)

Maradudin et al.  
(Laguerre function expansion)

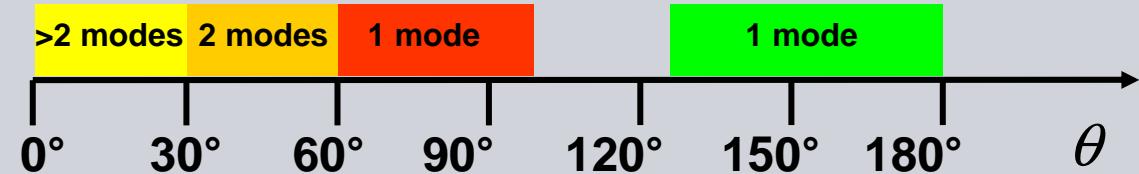


Findings for isotropic medium in Poisson case ( $\lambda = \mu$ ):



Odd (flexural) modes

Even modes  
(weakly localized)



# Evolution Equation

for even wedge modes:

$$i \frac{\partial}{\partial \tau} B(q) = q^2 \Delta_w(q) B(q)$$

$$+ q v_w \left[ \int_0^q F\left(\frac{k}{q}\right) B(k) B(q-k) dk + 2 \int_q^\infty \left(\frac{q}{k}\right)^2 F\left(\frac{q}{k}\right)^* B(k) B(k-q)^* dk \right]$$

(Krylov, Parker)

# Summary

- Theoretical description of nonlinear acoustic pulse evolution on solid surfaces
- Strong influence of anisotropy on nonlinear pulse evolution
- Frequency up-conversion relative to down-conversion more efficient than in case of BAWs,  
(would be even more efficient in 1D acoustic waveguides)
- Solitary SAW and solitary edge pulses exist.  
They are not solitons.

# Cooperations



**Christian Eckl**

University of Regensburg &  
Infineon AG, Munich

**Alexander S. Kovalev**

Institute for Low Temperature Physics  
and Engineering, Kharkov

**Alexey M. Lomonosov**

General Physics Institute, Moscow &  
University of Heidelberg

**Peter Hess**

University of Heidelberg