

# Half-Integer Shapiro Steps at the $0-\pi$ Crossover of a Ferromagnetic Josephson Junction

- Investigation of current phase relation (CPR) of SFS junctions near the crossover between the  $0$  and the  $\pi$  ground state (driven both by thickness and temperature)
- At a certain thickness (17 nm) a nonzero critical current is observed which is analyzed by a high frequency excitation  
     $\Rightarrow$  observation of half-integer Shapiro steps
- These half-integer steps are attributed to the doubling of the Josephson frequency due to a  $\sin(2\gamma)$  component of the CPR explained by level splitting of the energy levels in the ferromagnetic exchange field

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# Outline of the talk

- Introduction to the RSJ-model
  - resistively (and capacitively) shunted junction (RCSJ)
  - mechanical analog
  - explanation of Shapiro steps
- Introduction to ferromagnetic Josephson junctions
  - quick review of energy level distribution
  - peculiarity of ferromagnetic junctions
  - $\pi$  state
- Half-integer Shapiro steps at the  $0$ - $\pi$  crossover of a ferromagnetic Josephson junction
  - setup
  - experiment
  - interpretation

# Introduction to the RSJ-model

- fundamental Josephson relations:

(1)

$$I_s = I_c \sin(\gamma)$$

$$\frac{d\gamma}{dt} = \frac{2eV}{\hbar} = \frac{2\pi V}{\Phi_0}$$

(2)

with  $\gamma$  being the gauge invariant phase

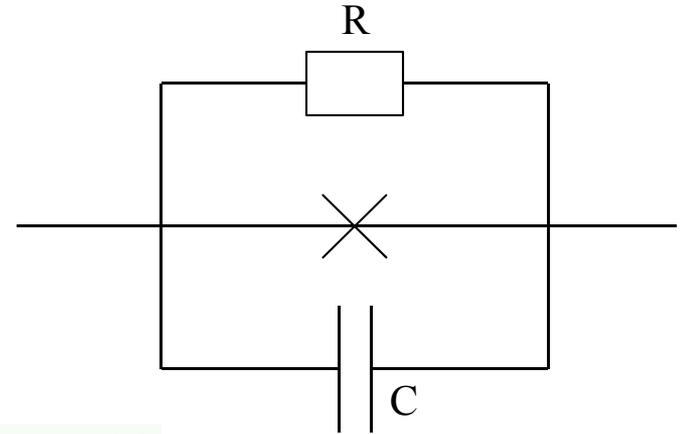
- (1) is sufficient for dc phenomena but for situation involving the ac Josephson effect (2) a more complete description is required
- model the physical Josephson junction by an ideal one described by (1), shunt  $\Rightarrow$  by a resistance R and a capacitance C

$\Rightarrow$  R builds in dissipation in finite voltage regime

C reflects the capacitance between the electrodes

## The RSJ-model

- equivalent circuit of the junction:
- the bias current is then given by:



$$I = I_c \sin(\gamma) + \frac{V}{R} + \frac{dV}{dt}$$

(3)

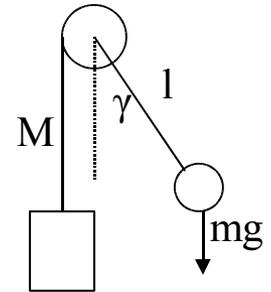
- replacing  $V$  in favor of  $\gamma$  using (2)  
one gets

$$I = I_c \sin(\gamma) + \frac{\Phi_0}{2\pi R} \dot{\gamma} + C \frac{\Phi_0}{2\pi} \ddot{\gamma}$$

(4)

- there exists only an analytic solution to this in the limit of  $C=0$  but one can understand the behavior qualitatively by considering a mechanical analog

# Mechanical Analog: The Physical Pendulum



- the equation of motion for a physical pendulum is

$$M = mgl \sin \gamma + \Gamma \dot{\gamma} + \Theta \ddot{\gamma} \quad (5)$$

with

$\Theta$ : momentum of inertia  
 $\Gamma$ : damping constant  
 $M$ : external torque

- the analogy is the given by identifying the angle  $\gamma$  with the gauge invariant phase
- the change in  $\gamma$  with time (angular velocity) corresponds to the voltage drop  $V$  over the Junction

Pendulum	Jos. Junction
$M$	$I$
$mgl$	$I_c$
$\Gamma$	$\Phi_0/(2\pi R)$
$\Theta$	$C\Phi_0/(2\pi)$

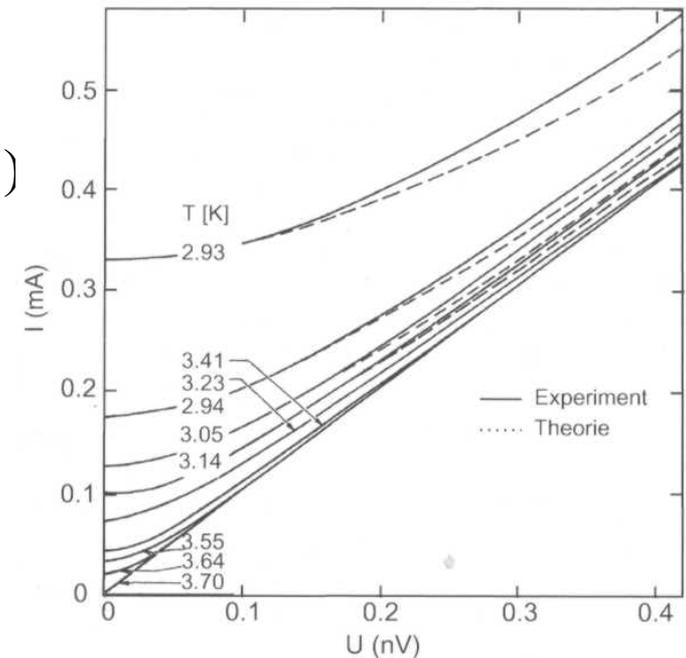
## Approximation: the overdamped case

- for most cases one can use the approximation  $RC \rightarrow 0$  yielding a first order nonlinear differential equation

$$\dot{\gamma} = \frac{mgl}{\Gamma} \left( \frac{M}{mgl} - \sin \gamma \right) \quad (6) \quad \dot{\gamma} = \frac{2\pi R I_c}{\Phi_0} \left( \frac{I}{I_c} - \sin \gamma \right) \quad (7)$$

- the time average voltage can be found by integrating over time and using the Josephson frequency relation (2) giving

$$V = R(I^2 - I_c^2)^{1/2} \quad (8)$$



# Remarks about numerical solution

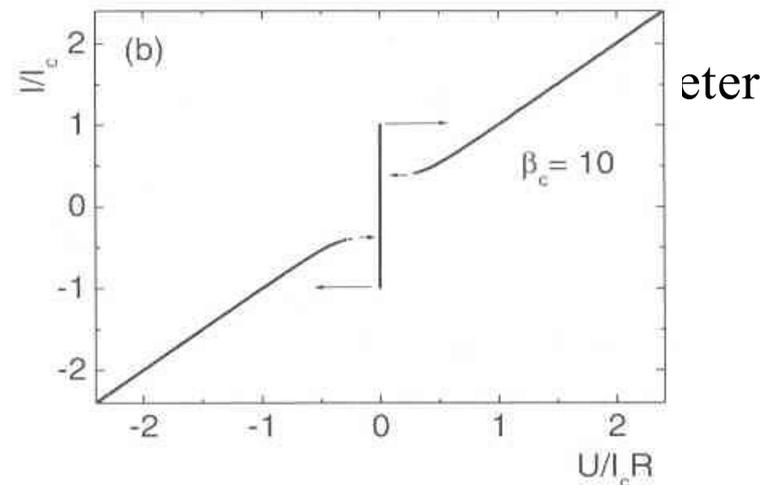
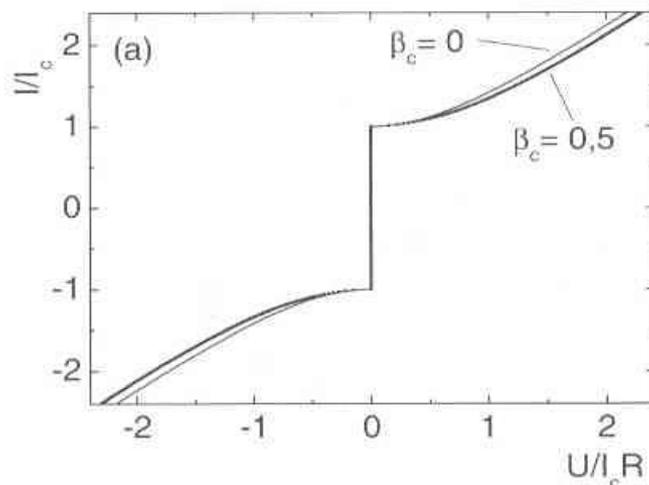
- the RSJ-model can of course be treated numerically for which occasion one usually defines one single dimensionless parameter using the characteristic values of the junction:  $V_c = I_c R$

$$\tau_c = \Phi_0 / 2\pi I_c R$$

$$f_c = 1/2\pi\tau_c$$

- with those one can write the differential equation in the compact form

$$i = \sin \gamma + \dot{\gamma} + \beta_c \ddot{\gamma}$$

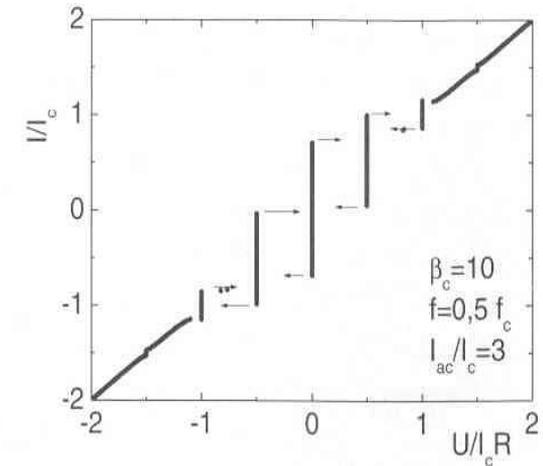
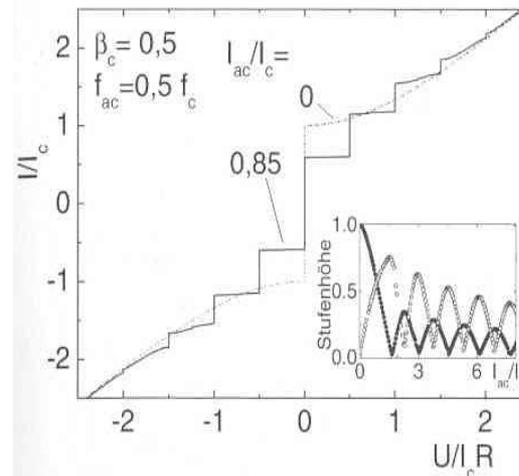


# rf-Driven Junctions

- mechanical analog: nonlinear oscillator is tuning its resonance to the driving frequency over a certain frequency interval
- so for one value of applied torque there's a range of values of angular velocities
- or similar for one value of angular velocities there is a range of torques that give that velocity
- for the Josephson junction this means that there will be the same voltage drop over the junction for a range of different bias current values

namely those that

- this leads to the Shapiro steps



## Quick glance at the calculation

- suppose the junction is biased with  $V = V_0 + V_1 \cos(\omega_1 t)$  then the time dependent phase is given by

$$\gamma(t) = \gamma_0 + \omega_0 t + \frac{2eV_1}{\hbar\omega_1} \sin \omega_1 t$$

(10)

which results in a CPR of  $I_s = I_c \sum (-1)^n J_n \left( \frac{2eV_1}{\hbar\omega_1} \right) \sin(\gamma_0 + \omega_0 t - n\omega_1 t)$

(11)

where  $J_n$  is the  $n$ th order Bessel function

- this contribute to a dc component only when  $\omega_0 V_n = n\hbar\omega_1/2e$  the dc voltage  $V_0$  has one of the Shapiro step values

$$I_n = I_c J_n(2eV_1/\hbar\omega_1)$$

(12)

- using (11) one can also deduce the half-width of the  $n$ th step

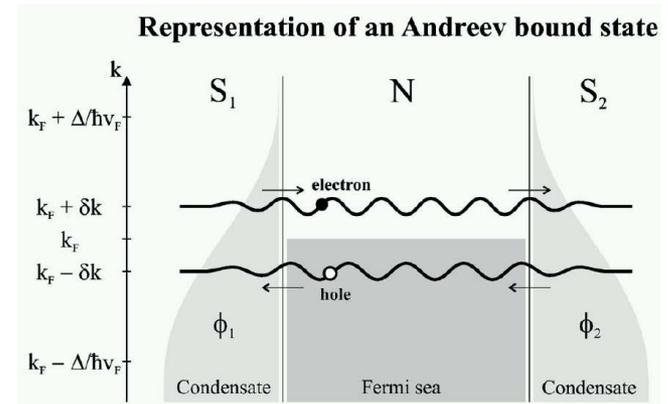
(13)

# Introduction to Ferromagnetic Josephson Junctions

- formation of bound states when the phase difference of the electron and the hole match the macroscopic phase difference of the superconducting wave functions
- in the ferromagnet an additional phase shift due to the exchange energy

$$q = E_{ex} / \hbar v_F$$

arises

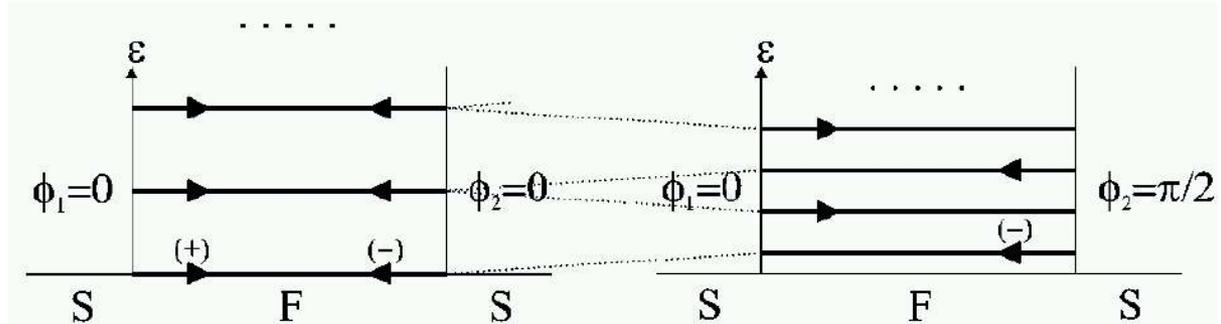


$$\begin{cases} k_e^\downarrow(\epsilon) = k_F - q + \delta k \\ k_h^\uparrow(\epsilon) = k_F + q - \delta k \end{cases}$$

$$\begin{cases} k_e^\uparrow(\epsilon) = k_F + q + \delta k \\ k_h^\downarrow(\epsilon) = k_F - q - \delta k \end{cases}$$

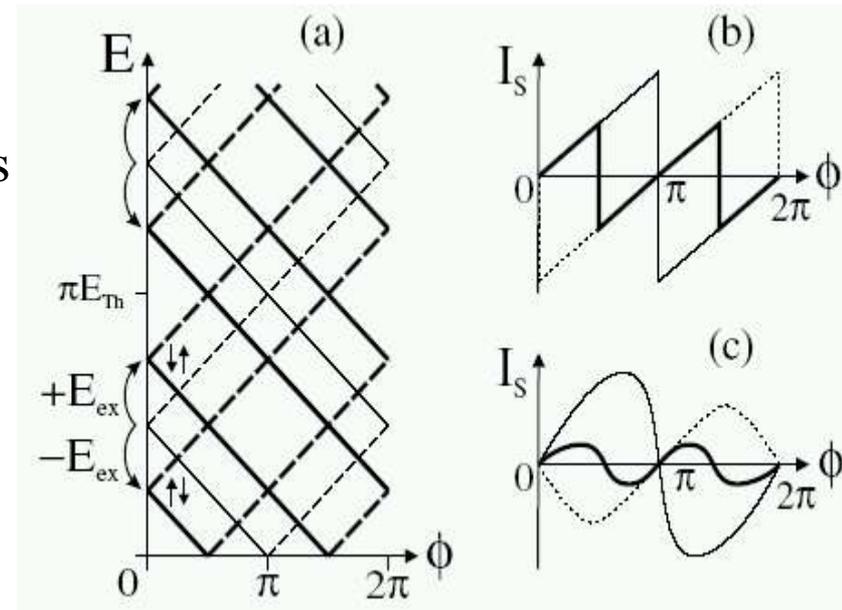
# Andreev bound states in SFS junctions

- In the ferromagnet the two spin directions of each bound state are indeed shifted by the exchange energy
- In the case that the exchange energy shifts the first level from finite energy to zero energy the direction of the lowest level is negative
- In this case the ground state is at  $\Phi=\pi$



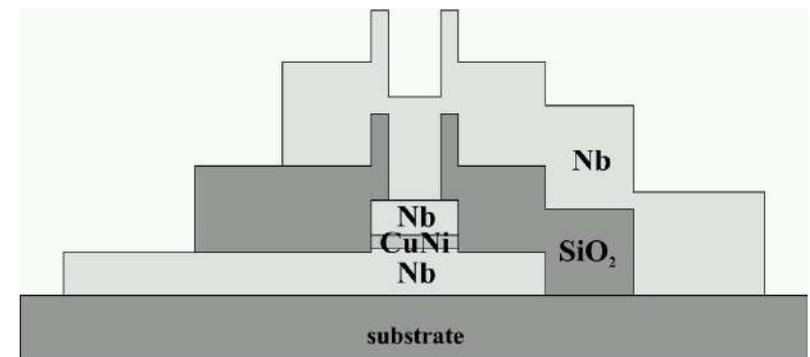
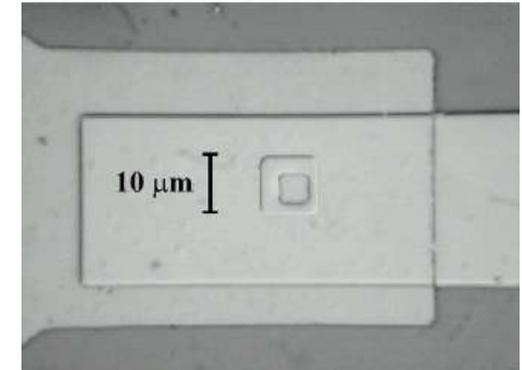
# Crossover from $0$ to $\pi$

- consider the situation where the exchange energy doesn't shift the first energy level completely to zero energy but only half-way
  - ⇒ the spectrum contains equidistant levels twice closer than usual
  - ⇒ the supercurrent is  $\pi$  periodic in phase
- at this  $0$ - $\pi$  crossover the CPR contains a dominant  $\sin(2\gamma)$  component and the critical current has a nonzero minimum with respect to thickness or exchange energy
- so far the critical current of SFS junctions at the crossover was assumed to vanish completely



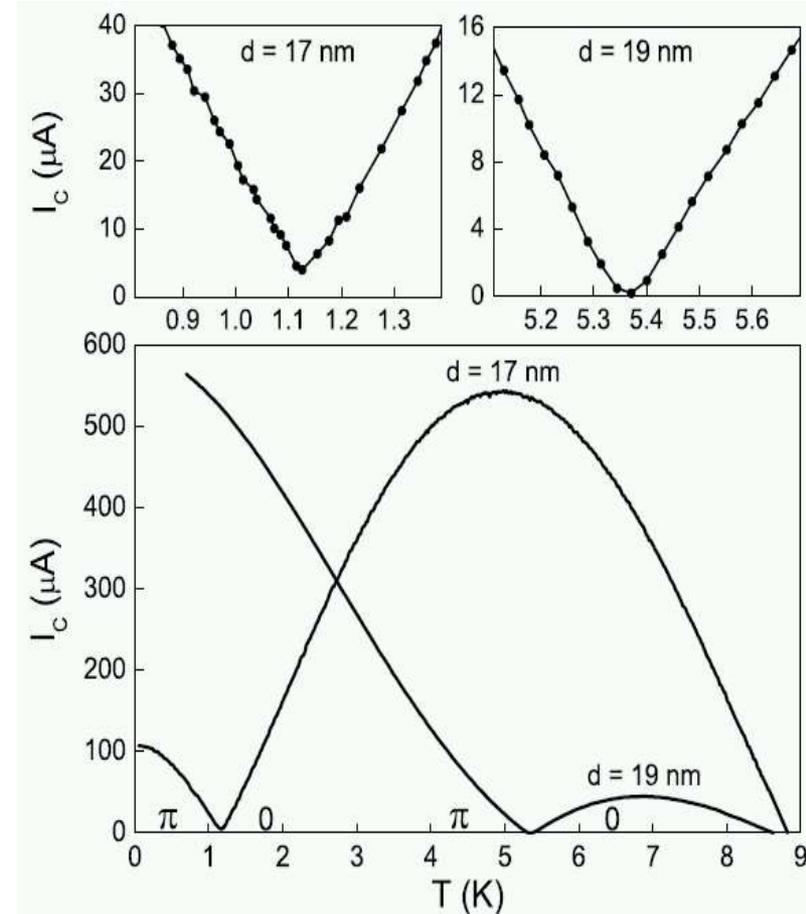
# Experimental Setup

- Nb/Cu<sub>52</sub>Ni<sub>48</sub>/Nb trilayers deposited in situ and patterned by photolithography
- $T_{\text{curie}} = 20\text{K}$
- the current through the junction is measured by a SQUID feedback method
- thicknesses of 17 and 19nm



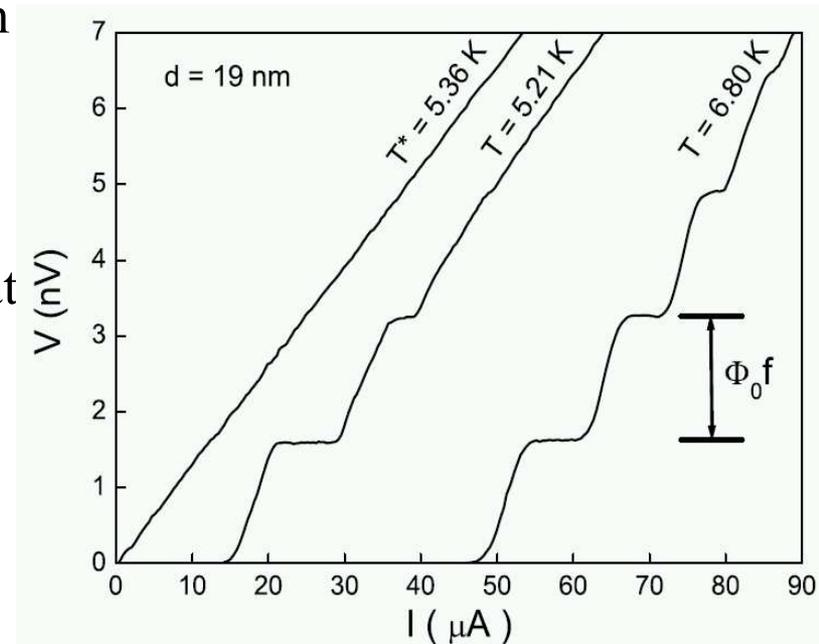
# Temperature dependence of critical current

- the critical current presents a deep minimum at  $T^*$ , the crossover temperature
- there exists a finite current of  $4\mu\text{A}$  at  $T^*$  for the 17nm thick junction
- with its crossover temperature so close to zero this junction is almost the optimum case where  $E_{\text{ex}}/E_{\text{th}}$  gives a doubled periodicity of Andreev levels



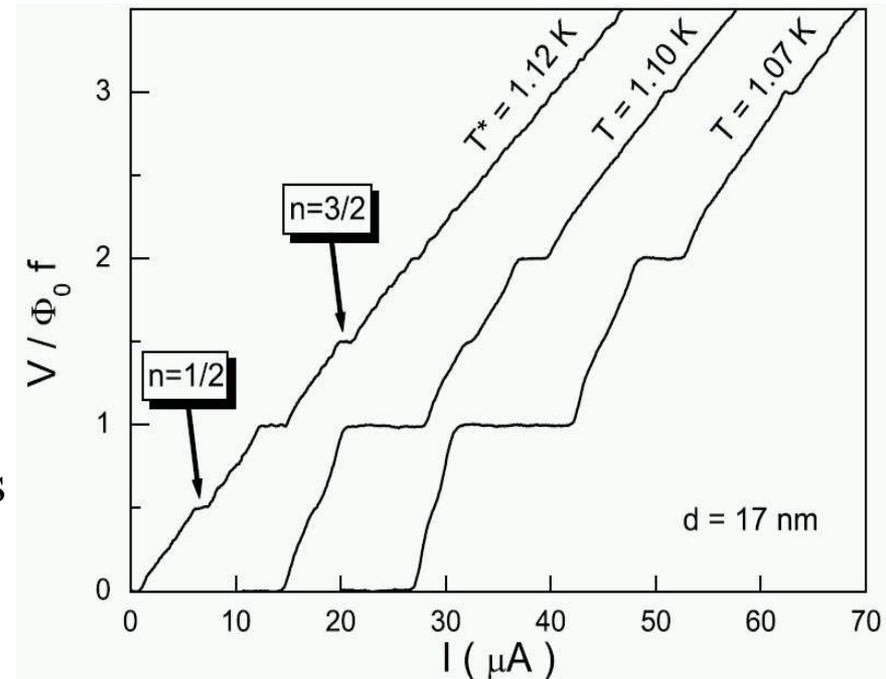
# Experiment for 19 nm

- the CPR is analyzed by sending an alternative current at  $f=800$  kHz through the junction when measuring the direct current-voltage curve
- constant voltage Shapiro steps appear due to the synchronization of the Josephson oscillations with the applied excitation
- as expected (by RSJ) the steps appear at voltages equal to  $V_n = n\Phi_0 f$
- no steps are present at the crossover temperature  $T^*(19\text{nm})=5.36\text{K}$



# Experiment for 17 nm

- in this case the steps are still present at  $T^*(17\text{nm})=1.12\text{K}$
- additional steps appear at  $n=1/2$  and  $n=3/2$
- the half-integer steps reveal the existence of supercurrent oscillations at a frequency of  $2(V/\Phi_0)$  which synchronize to the excitation at frequency  $f$  producing steps at voltage multiples of  $1/2(\Phi_0 f)$



## Discussion of results 1

- ideally the  $\sin(2\gamma)$  component should dominate for this thickness of junction at all temperatures  $T \ll T_c$
- the fact that they are visible only close to the crossover temperature  $T^*$  indicates that the phase dependence departs only slightly from  $\sin(\gamma)$
- the  $\sin(2\gamma)$  component dominates only when the large  $\sin(\gamma)$  cancels to change its sign
- to first order near  $T^*$  the supercurrent can be described by

$$I_s(\gamma) = \frac{T - T^*}{T^*} I_1 \sin \gamma + I_2 \sin 2\gamma$$

(16)

- in contrast to other situations with half-integer steps they only appear here because of

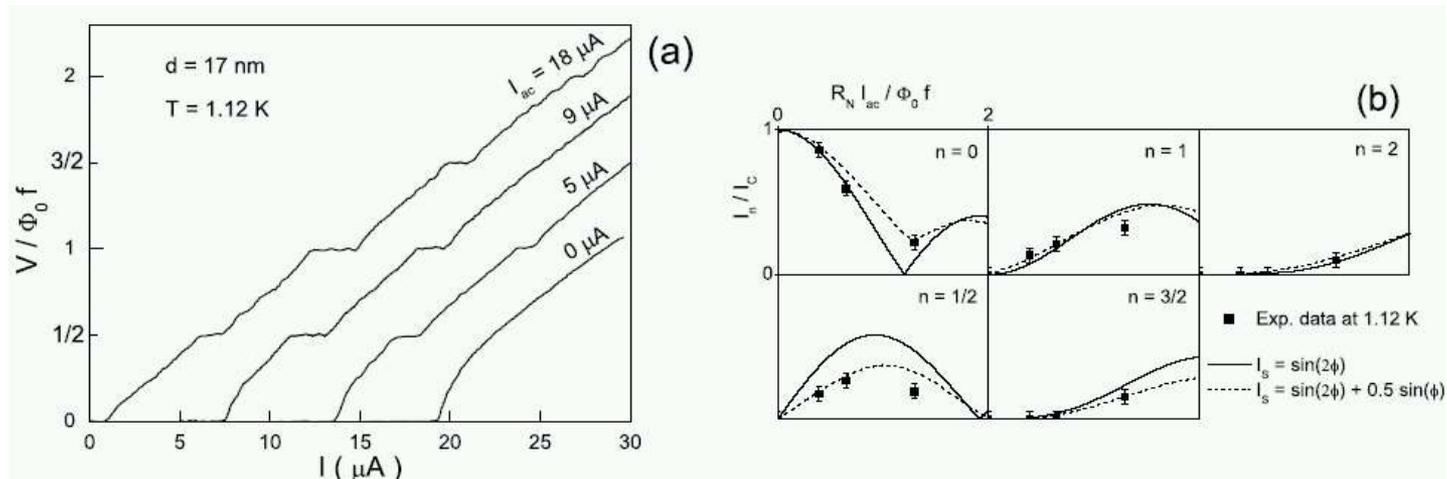
the crossover

the low temperature

the finite critical current

## Discussion of results 2

- investigation of spectral composition in greater detail by applying different excitation amplitudes (18, 9, 5, and 0  $\mu\text{A}$ ) at  $d = 17$  nm and  $T = T^* = 1.12$  K
- comparison of the Shapiro step widths to different RSJ-model predictions



- the best fit of the experimental data is achieved with a spectral composition of  $I_s = \sin(2\gamma) + 1/2\sin(\gamma)$

# Summary

- the study of the finite voltage behavior of SFS junctions under high frequency excitation revealed half-integer Shapiro steps at the crossover temperature where the critical current is nonzero
- the steps show the  $\sin(2\gamma)$  dependence of the current phase relation which can be explained by specific level splitting realized at the crossover

- CPR of tunnel junctions:

$$I_s = I_c \sin(\gamma)$$

(14)

- CPR of SNS or SFS junctions are predicted to be nonsinusoidal:

$$I_s(\gamma) = \sum_{n=1}^{\infty} I_c^{(n)} \sin n\gamma$$

(15)

due to a different conduction mechanism explained by Andreev bound states

- additionally the CPR in SFS junctions is strongly distorted by the exchange field of the ferromagnet and can even be reversed